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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification⁶ : B60R</p>	<p>A2</p>	<p>(11) International Publication Number: WO 00/00365 (43) International Publication Date: 6 January 2000 (06.01.00)</p>
<p>(21) International Application Number: PCT/US99/07049 (22) International Filing Date: 17 May 1999 (17.05.99) (30) Priority Data: 09/094,406 10 June 1998 (10.06.98) US (71) Applicant: ATLANTIC RESEARCH CORPORATION [US/US]; 5945 Wellington Road, Gainesville, VA 20155-1699 (US). (72) Inventors: LUNDSTROM, Norman, H.; 8140 Bayonet Way #101, Manassas, VA 22701 (US). GRESO, Aaron, J.; 600 Friendship Way #102, Culpeper, VA 22701 (US). SCHEFFEE, Robert, S.; 9450 Jerico Court, Lorton, VA 22079 (US). (74) Agent: PRESTA, Frank, P.; Sixbey, Friedman, Leedom & Ferguson, P.C., Suite 800, 8180 Greensboro Drive, McLean, VA 22102 (US).</p>		<p>(81) Designated States: CA, JP, KR, MX, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>Without international search report and to be republished upon receipt of that report.</i></p>
<p>(54) Title: PYROTECHNIC GAS GENERANT COMPOSITION INCLUDING HIGH OXYGEN BALANCE FUEL (57) Abstract A pyrotechnic gas generant composition includes a high oxygen balance compound or fuel, preferably, azodiformamidine dinitrate, which is the resulting reaction product of an aminoguanidine salt and nitric acid. Specifically, the high oxygen balance compound or fuel of the present invention is the resulting reaction product of aminoguanidine salts, such as aminoguanidine nitrate, aminoguanidine bicarbonate, or aminoguanidine sulfate with nitric acid. Preferably, the aminoguanidine salt is aminoguanidine bicarbonate. The resulting reaction product is a yellow precipitate that can be used alone, with or without oxidizers or other additives, for very rapid self-deflagration or in combination with oxidizers and additives. In each instance, the gas generant composition provides both high gas output and low production of solid combustion products. Further, the precipitant is relatively non-hygroscopic and has a high burn rate. The gas generating composition is useful as a gas generator for an air bag of an occupant restraint system for an automobile, gun propellants, inflation and expulsion devices, flotation devices, pyrotechnics, fire suppression devices and smokeless, reduced smoke and smokey rocket propellants.</p>		

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**PYROTECHNIC GAS GENERANT COMPOSITION INCLUDING
HIGH OXYGEN BALANCE FUEL**

BACKGROUND OF THE INVENTION

1. FIELD OF THE INVENTION

The present invention relates to ingredients for use in pyrotechnic gas generant compositions, and more specifically to fuels containing a high oxygen balance. The gas generant compositions are useful as gas generant propellants for air bag occupant restraint systems for automobiles, gun propellants, inflation and expulsion devices, flotation devices, ignition materials, pyrotechnics, fire suppression devices and smokeless and smoke producing rocket propellants.

2. BACKGROUND ART

There is high demand for pyrotechnic gas generant compositions which on combustion yield acceptable burning rates and provide, at relatively low flame temperatures, a high volume of substantially non-toxic gas and a low volume of solid particulate matter that can produce smoke. It is also important that resulting solid by-products from the combustion of gas generant compositions be minimal, and the gaseous combustion products be substantially non-toxic, and non-corrosive. Various compositions of gas generants have been utilized in the past in an attempt to reach the above desirable characteristics.

U.S. Patent No. 3,405,144 discloses a 1-azido-N,N,N'-trifluoroformamidine that is useful in a propellant composition which exhibits a high specific impulse. Specifically, the said material is disclosed to be useful in rocket fuel compositions.

Gas generant compositions have also been developed to include the addition of modifiers to lower flame temperatures and increase gas production. Further ingredients may be added such as binders, ignition aids, slag formers, scavengers, and catalysts to improve various features

of the underlying propellant. The modifiers and additional ingredients often times, however, improve one aspect of the propellant composition while also contributing to the production of undesirable by-products and may increase the corrosiveness thereof. This is particularly disadvantageous in an automobile air bag environment.

One major gas generating composition having desirable characteristics contains strontium nitrate and 5-aminotetrazole (SrN/5ATZ) as major constituents. This formulation is relatively non-toxic when compared with sodium azide systems, has good ballistic properties and retains the majority of solid combustion products as a slag or clinker either in the combustion or filtration areas of, for instance, an air bag system for an automobile. These formulations also exhibit acceptable flame temperatures of 2250°K to 2750°K depending upon the stoichiometry of the formulation and the oxygen to fuel ratio. Moreover, the strontium nitrate and 5-aminotetrazole formulations are relatively non-hygroscopic and the ingredients do not exhibit crystalline phase changes over the operating temperature range of the air bag system.

Such a formulation, however, suffers with regard to gas output, specifically, in the volume limited systems of a driver's side air bag. This is because a high concentration of strontium nitrate is required to maintain a neutral oxygen to fuel (O/F) balance. Because inflator designs are becoming smaller and smaller and, thus, more volume limited, propellants are required to provide greater gas output and still retain the desirable attributes of the strontium nitrate/5-aminotetrazole systems.

Approaches have been taken to obtain the attractive features of the above-noted propellants, while overcoming the low gas output thereof. This has resulted in the development of propellants based on mixtures of potassium perchlorate and oxygenated fuels such as guanidine nitrate and aminoguanidine nitrate. These propellants are also relatively non-hygroscopic, provide excellent gas output, high burning rates and only

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about two thirds of the solid combustion products of the above-noted strontium nitrate and 5-aminotetrazole based propellants. Unfortunately, the solid combustion products do not form clinkers or slags which deposit in the combustion or filtration area, but instead form very fine particulates in the gas stream which results in a smokey and dirty exhaust.

Smoke or dirty exhaust combustion products are not commercially desirable, particularly, in automobile air bag systems since the production of such product may cause undue anxiety on the part of drivers and passengers involved in an automobile accident in which air bags are deployed. As a result, there is a need for a propellant material or gas generant that exhibits high gas output upon combustion, but does not produce unwanted by-products upon combustion.

SUMMARY OF THE INVENTION

The object of the present invention is to improve upon and to overcome the deficiencies of the prior art and to provide a substantially non-hygroscopic, substantially non-toxic gas producing pyrotechnic gas generant composition that upon combustion produces a high gas output and a high burn rate with limited non-gaseous combustion products.

Another object of the present invention is to provide a pyrotechnic gas generant composition including a high oxygen balance fuel, preferably, azodiformamidine dinitrate, that produces the desirable high gas output at a low combustion temperature and reduced non-gaseous combustion products.

Still another object of the present invention is to provide a pyrotechnic gas generant composition including a high oxygen balance fuel, preferably, azodiformamidine dinitrate, with the capability of self-deflagration similar to a solid monopropellant.

Yet another object of the present invention is to provide a pyrotechnic gas generant composition including a high oxygen balance fuel which will auto-ignite in an inflator at acceptable but low enough

temperatures to ensure that the inflator only rupture but does not fragment in a bonfire test.

Still another object of the present invention is to provide a gas generating composition capable of producing a substantially high gas output upon combustion for use as an automobile air bag propellant. However, the composition of the present invention may also be employed to inflate such items as an inflatable raft or passenger escape chute of an airplane, as well as for gun propellants, pyrotechnics, ignition mixtures, fire suppression devices and rocket propellants. From a practical standpoint, the composition of the present invention also may include additives heretofore used with other gas generant compositions, such as oxidizers, gas conversion catalysts, ballistic modifiers, slag formers, ignition aids, energetic plasticizers and binders, non-energetic binders, and compounding aids.

The foregoing objects are generally achieved by a pyrotechnic gas generant composition including a high oxygen compound or fuel, preferably, azodiformamidine dinitrate, which is the resulting reaction product of aminoguanidine nitrate and nitric acid prepared with or without the use of potassium permanganate. Specifically, the reaction product is a yellow precipitate that can be ignited and used alone, with no oxidizers or other additives, for very rapid and substantially smokeless self-deflagration or combusted in combination with oxidizers and/or other additives. In each instance, the gas generant composition provides both high gas output and low production of solid decomposition products upon combustion. Further, the precipitate is relatively non-hygroscopic and has a high burn rate. As a result, cartridges used to contain the gas generating composition are not required to withstand the extremely high pressures associated with prior art gas generating compositions, such as ammonium nitrate based compositions, that exhibit the similar low solid combustion

product production as the gas generating composition of the present invention, but have low burn rates and are generally hygroscopic.

Based upon the general physical characteristics of the above-noted reaction product of the present invention, the product is believed to be 1,1'-azodiformamidine dinitrate. However, the pyrotechnic gas generant composition of the present invention is directed separately to both the use of the yellow reaction product of aminoguanidine nitrate and nitric acid and to 1,1'-azodiformamidine dinitrate.

The azodiformamidine dinitrate may also be formed as the reaction product of nitric acid and other aminoguanidine salts, such as aminoguanidine bicarbonate, aminoguanidine sulfate, or any combination thereof. Preferably, the aminoguanidine salt is aminoguanidine bicarbonate. The use of such materials provide a cost effective means of producing the azodiformamidine dinitrate of the present invention.

The gas generant composition of the present invention is generally prepared by the methods heretofore employed for prior art compositions and generally, but not exclusively, involve the dry or wet blending and compaction of the comminuted ingredients selected for combination. In view of the advantageous characteristics of the gas generant composition of the present invention, namely, high gas output, low solid combustion products production and high burn rate, the generant has applications in automobile air bag systems, inflatable rafts or passenger escape chutes, gun propellants, pyrotechnics, ignition mixtures, fire suppression devices and rocket propellants.

For purposes of the present invention, the terms propellant(s) and gas generant(s) are used interchangeably. Also, for the purposes of this invention, the reactions shown are with anhydrous components. The use of non-anhydrous components, however, is also contemplated.

BRIEF DESCRIPTION OF THE FIGURES

Figure 1 is a conventional passenger-side inflator that may be used with the composition of the present invention.

Figure 2 is a conventional driver-side inflator that may be used with the composition of the present invention.

Figure 3 is an infrared absorption spectra of the reaction product of embodiment 1 of the present invention.

Figure 4 is a differential scanning calorimetry of the reaction product of embodiment 1 of the present invention.

Figure 5 is a differential scanning calorimetry of the reaction product of embodiment 2 of the present invention.

Figure 6 is a differential scanning calorimetry of the reaction product of embodiment 3 of the present invention.

Figure 7 is an infrared absorption spectra of the reaction product of embodiment 1 of the present invention.

Figure 8 is an infrared absorption spectra of the reaction product of embodiment 2 of the present invention.

Figure 9 is an infrared absorption spectra of the reaction product of embodiment 3 of the present invention.

Figures 10(a)-(d) are infrared absorption spectra of the reaction product of embodiments 4, 1, 2 and 3, respectively, of the present invention.

Figure 11 is a prior art infrared absorption spectra for azodicarbamidine dinitrate.

Figure 12 is a graph showing a representative firing of the reaction product of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

The invention provides for a pyrotechnic gas generant, preferably comprising azodiformamidine dinitrate, which when combusted provides

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high gas output and minimal solid combustion products and which is useful for various purposes. It has been found that the reaction of the high oxygen balance fuel of the present invention with an oxidizer produces a high gas output volume with very little solid combustion products. In addition, the fuel, preferably azodiformamidine dinitrate, also exhibits a high burn rate and is a self-deflagrating monopropellant. As a result, the gas generant composition of the present invention can be a single ingredient auto-ignition pill (AIP); a solid monopropellant; a high oxygen balance fuel in all pyro systems; a burning rate enhancing additive; and an ingredient in conventional and oxygenated hybrid inflation systems. As one can see, the gas generant of the present invention is particularly useful as an automobile air bag propellant, but also has applications as a gun propellant, flotation device gas generant, propellant, pyrotechnic, gas generator, ignition mixture, fire suppression device and rocket propellant.

Additional objects and advantages of the present invention will become readily apparent to those skilled in the art from the following detailed description wherein the preferred embodiments of the invention are shown and described simply by way of illustration of the best mode contemplated for carrying out the invention. As will be realized, the invention is capable of other and different embodiments and its several details are capable of modifications of various obvious respects, all without departing from the invention. Accordingly, the figures and description are to be regarded as illustrative in nature and not as restrictive.

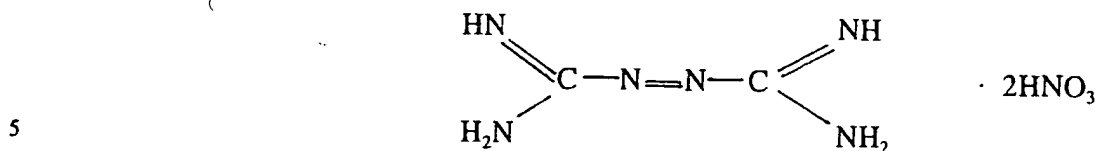
More specifically, the gas generant composition of the present invention includes a high oxygen balance formamidine-type fuel prepared from the reaction of nitric acid and aminoguanidine nitrate. The inventors believe the fuel - to be azodiformamidine dinitrate (also called

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azodicarbamidine dinitrate, azobicarbamidine dinitrate, and azobisformamidine dinitrate) shown structurally as follows:



This invention is not limited, however, to only azodiformamidine dinitrate, both crystallized and recrystallized, but instead is also directed to the product from the reaction of nitric acid and aminoguanidine nitrate as provided in detail below.

10 The gas generant composition of the present invention may also be formed from the reaction of nitric acid and other aminoguanidine salts, such as aminoguanidine bicarbonate (AGB) or aminoguanidine sulfate (AGS). Preferably, the aminoguanidine salt is AGB. The product from the reaction of these salts with nitric acid similarly produces a solid, bright
15 yellow colored material believed to be azodiformamidine dinitrate as noted above with respect to the reaction of nitric acid and aminoguanidine nitrate.

With regard to azodiformamidine dinitrate, reference is made to J.Thiele, Ann 270, 39 (1892) which describes this compound as azodicarbonamidinnitrat. This previous synthesis was done in conjunction
20 with an investigation of materials for potential woolen dyes/pigments.

Moreover, the prior synthesis involved the addition of a solution of a metallic oxidizing compound (potassium permanganate) to form a yellow reaction product and did not add heat from an external source during the process. The method of the present invention, as provided below, is
25 preferred because by adding heat, the reaction occurs rapidly without requiring the addition of a metal oxidizing compound. By avoiding the use of a metal oxidizing compound during the preparation of the yellow reaction product, the high oxygen fuel gas generant of the present invention can be prepared free of foreign solid minute particles or without the
30 potential for formation of metallic oxide particles. Thus, gas generants

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using the high oxygen balance fuel of the present invention can be prepared without metal-containing contaminants.

In accordance with the present invention, the reaction to form azodiformamidine dinitrate will also occur without external heat and with or without the use of potassium permanganate at ambient temperature if nitric acid and aminoguanidine nitrate are allowed to digest over a longer period of time. This also applies to the use of the above-identified additional salts, namely, aminoguanidine bicarbonate (AGB) and aminoguanidine sulfate (AGS).

Other high oxygen balance fuels hydrazodicarbonamidine, diazoguanidine, formamidine, bisformamidine, and azobisformamidine derivative fuels such as guanyl azide nitrate, diazoguanidine nitrate, azobisnitroformamidine, and 1,1'-azodiformamidine dipicrate are also useful gas generator ingredients in accordance with the present invention. In addition, other derivatives and fuels containing a formamidine, guanyl azide, diazoguanidine, or hydrazodicarbonamidine group with an oxidizing group, e.g. (NO₂), (NO₃), (ClO₄), (ClO₃), or mixtures of oxidizing groups, or mixtures of different hydrazodicarbonamidine, guanyl azide, diazoguanidine, formamidine, bisformamidine, and azobisformamidine compounds, with oxidizing groups with proper precautionary measures, are also useful in propellant compositions.

Prior art propellants, such as those containing ammonium nitrate, produce very little solid combustion products, but have a number of other properties that make them less desirable. Ammonium nitrate, for instance, is hygroscopic. Moreover, in gas generant/propellant compositions, its use results in a low burn rate and a high pressure exponent at operating pressures of 1000-2000 psi. Consequently, a propellant composition including ammonium nitrate as the principal oxidizer must be burned at very high pressures, e.g. 4000-6000 psi, and sealed to prevent moisture from contacting the composition. In addition, ammonium nitrate typically

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requires the use of phase stabilizers, such as potassium compounds, which generate solid combustion products.

The high oxygen balance fuel of the present invention overcomes a number of the above-noted, less than desirable characteristics. Specifically, a gas generant/propellant composition including the high oxygen balance fuel of the present invention exhibits a high gas output with no or little resulting solid combustion product or ash, while also being relatively non-hygroscopic, having a high burn rate and providing a more desirable pressure exponent. As a result, the composition of the present invention does not have to be held in such a high pressure and moisture sealed container, since the operating pressures required for achieving burning rates are much lower than for the above-noted ammonium nitrate gas generant propellant compositions.

The gas generant composition of the present invention can function alone as a self-deflagrating monopropellant, as noted above, or include an oxidizer. Other materials may be added to the composition for processing, aiding ignition, enhancing ballistics, improving thermal aging and stability, improving hazardous properties, reducing particulates, binding, and scavenging undesirable gaseous combustion products.

A single oxidizer or multiple oxidizers may be combined with the high oxygen balance fuel of the present invention to supply additional oxygen for achieving the desired oxygen to fuel balance (O/F) during combustion. Since the high oxygen balance fuel of the present invention includes a larger amount of oxygen than prior gas generating compositions, a smaller amount of oxidizer for providing a desirable oxygen to fuel (O/F) balance is necessary. Suitable metallic and non-metallic oxidizers are known in the art and generally comprise nitrites, nitrates, chlorites, chlorates, perchlorates, oxides, hydroxides, peroxides, persulfates, chromates and perchromates of non-metals, alkali metals, alkaline earth metals, transition metals and transition metal complexes and mixtures

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thereof. Preferred oxidizers include ammonium perchlorate, potassium perchlorate, strontium nitrate, potassium nitrate, sodium nitrate, barium nitrate, potassium chlorate, and mixtures thereof.

Preferred oxidizers are non-hygroscopic in order to preserve the advantageous characteristic of the high oxygen balance fuel of the present invention. The preferred oxidizers are generally employed in a concentration of about 0% to 98% by weight of the total gas generant composition and preferably in a concentration of 5 to 50% by weight of the total gas generant composition.

Scavengers may be desirable to control the production of corrosive combustion products. For example, if a non-metal oxidizer is used, such as ammonium perchlorate, hydrogen chloride (HCl) can be produced as a resulting reaction product, which is clearly undesirable. To prevent the production of HCl, a scavenger such as sodium nitrate can be used to form sodium chloride (NaCl) instead. Other corrosive/toxic gas scavengers may also be employed.

The combustion of the high oxygen balance fuel of the present invention may also be controlled by the addition of ballistic modifiers and include burning rate catalysts which influence the temperature sensitivity, pressure exponent and rate at which the propellant burns. Such ballistic modifiers were primarily developed for solid rocket propellants, but have also been found useful in gas generants for inflatable devices. Examples of ballistic modifiers useful with the composition of the present invention include oxides and halides of Group 4 to 12 of the Periodic Table of Elements (as developed by IUPAC and published by the CRC Press, 1989); sulfur and metal sulfides; transition metal salts containing copper, chromium, cobalt, nickel and mixtures thereof; and alkali metal and alkaline earth metal borohydrides. Guanidine borohydrides and triaminoguanidine borohydrides have also been used as ballistic modifiers. Organometallic ballistic modifiers include, but are not limited to, metal

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chelates, oxalates, metallocenes, ferrocenes and metal acetyl acetonates. Other ballistic modifiers include salts of dicyanamide, nitroguanidine, guanidine chromate, guanidine dichromate, guanidine trichromate, and guanidine perchromate. The ballistic modifiers are generally employed in concentrations varying from about 0.1 to 25% by weight of the total gas generant composition. Because of the self-deflagrating, high burning rate characteristics of the high oxygen fuel of the present invention, low concentrations of said fuel, namely, 0.1-25% can be incorporated for use as a ballistic modifier in other gas generant compositions.

Filterable slag formation can be enhanced by the addition of a slag former. Such a slag former may not, however, be necessary in the present invention in view of the limited amount of solid combustion product produced. Suitable slag formers, if deemed necessary, include lime, borosilicates, vycor glasses, bentonite clay, silica, alumina, silicates, aluminates, transition metal oxides, alkaline earth compounds, lanthanide compounds, and mixtures thereof.

Another additive found to aid in the ease and temperature of ignition and resulting combustion of gas generant compositions is an ignition aid. Ignition aids include finely divided elemental sulfur, boron, boron-potassium nitrate (BKNO_3), carbon, magnesium, aluminum, and Group 4 transition metals, transition metal oxides, hydrides and sulfides, the hydrazine salt of 3-nitro-1,2,4-triazole-5-one and mixtures thereof. The ignition aids are normally employed in concentrations of 0.1 to 15% by weight of the total gas generant composition.

It may be desirable to add compounding agents to facilitate compounding and obtain homogeneous mixtures. Suitable binders and processing or compounding aids include molybdenum disulfide, graphite, boron nitride, alkali metal, alkaline earth and transition metal stearates, various solvents, such as water, methanol, ethanol, ethyl ether, acetone, isopropanol, methylene chloride, etc, polyethylene glycols, polyacetals,

polyvinyl acetates, polyvinyl alcohols, polycarbonates such as Q-PAC, cellulose acetate (CA), cellulose acetate butyrate (CAB), cellulose nitrate (CN), fluoropolymers commercially available under the tradename TEFLON, and silicones. The compounding aids are typically, but not
5 universally, employed in concentrations of about 0.1 to 15% by weight of the total gas generant composition.

In addition to the above-noted additives, the high balance fuel of the present invention may also be combined with other fuels and/or energetic
10 nitro and/or nitrate plasticizers and/or energetic and non-energetic binders to provide a gas generant/propellant composition. Suitable fuels for such combination with the fuel of the present invention include but are not limited to the families of azido, hydrazine, guanidine, tetrazole, triazole, triazine, polyamine, nitramine (linear and cyclic), and derivatives of these
15 families of fuels, as well as mixtures thereof. Suitable energetic plasticizers include but are not limited to butanetriol trinitrate (BTTN), nitroglycerine (NG), triethyleneglycol dinitrate (TEGDN), trimethylolethane trinitrate (TMETN) and mixtures thereof. An example of an energetic binder includes glycidyl azide polymer (GAP).

The manner and order in which the components of the gas generant
20 composition of the present invention are combined and compounded are not critical so long as an intimate, uniform mixture with good structural integrity is obtained and the compounding is carried out under conditions which are not unduly hazardous, and, which do not cause decomposition of the components employed. For example, the materials may be wet
25 blended in aqueous or nonaqueous liquids, or dry blended, with or without binders or processing aids, in a ball mill or "RED DEVIL" type paint shaker and then extruded, pelletized by compression molding, or formed into a castable or compression molded monolithic grain. The materials
30 may also be ground separately or together with or without binders and/or other additives in a fluid energy mill, "SWECO" vibroenergy mill, or

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bantam micro-pulverizer and then blended or further blended in a v-blender prior to compaction.

The various components described hereinabove for use with the novel high oxygen balance fuel of the present invention have been used heretofore in other gas generant compositions. References involving gas generant compositions describing various additives include U.S. Patents No. 5,035,757; 5,084,118; 5,139,588; 4,948,439; 4,909,549; and 4,370,181. As taught in this art and as will be apparent to those skilled in the art, it is possible to combine the functions of two or more additives into a single composition. Thus, alkaline earth metal salts of tetrazoles, bitetrazoles and triazoles not only function as gas generant components but can also be used as slag formers. It has also been found that strontium nitrate, for instance, acts not only as an oxidizer and a slag former, but also is effective as a ballistic modifier, ignition aid, densifier and processing aid.

The high oxygen balance fuel of the present invention can utilize conventional gas generator mechanisms of the prior art. These are referred to in U.S. Patent No. 4,369,079, incorporated herein by reference. Generally, the methods of the prior art involve the use of a hermetically sealed metallic cartridge containing a gas generant composition. Hydrazodicarbonamidine, diazoguanidine, formamidine, bisformamidine, and azobisformamidine type fuels of the present invention can be used in such devices. Specifically, upon initiation of combustion by the firing of a squib, the sealing mechanism ruptures. This allows gas to flow out of the combustion chamber through several orifices. Of course, other gas generator mechanisms may equally be employed for use with the gas generant composition of the present invention.

With reference to an automobile air bag environment, Figure 1 depicts a conventional passenger-side hybrid inflator for an automobile in which the high oxygen balance fuel of the present invention may be used.

In practice, the initiator 1 ignites in response to a sensor (not shown) that senses rapid deceleration indicative of a collision. The initiator gives off hot gases that ignite the ignition charge 2 which causes the main generant charge 8 to combust, thereby heating and further pressurizing the inflation gas mixture 3. When the pressure in the inflation gas mixture increases to a certain point, the seal disk 6 ruptures, permitting the gas mixture to exit the manifold 4 through the outlet portions 5 and inflate an air bag. The generant container 9 holds the main generant charge 8. All the charges in the inflation gas mixture are enclosed in the pressure tank 7.

Figure 2 illustrates an all pyrotechnic gas generator in which the instant invention may be employed. Since no part of the inflator is reserved for storage capacity, the device is smaller than its counterpart hybrid inflator. In this figure, there is an initiator 11 that will combust in response to a signal from a sensor (not shown), that generates a signal as a result of a change in conditions, e.g., an excessive increase in temperature or a sudden deceleration of a vehicle (indicative of a crash), in which the inflator is installed. The initiator 11 gives off hot gases that ignite the main generant charge 16, which combusts, generating an inflation gas mixture. The mixture exits the manifold 14 through the exit ports 15. To insure that the gas generating propellant 16 will be ignited well below its auto-ignition temperature (T_{ig}) and well below that temperature where the materials of construction of the hardware begin to weaken, an auto-ignition propellant (AIP) 13 having a suitably low T_{ig} may be needed to ignite the ignition charge 12, which then ignites the propellant 16.

Because of the high burning rates exhibited by the high oxygen balance fuel of the present invention at moderate to low operating pressures, the invention may also be utilized in the physical form of a monolithic grain.

Use of the high oxygen balance fuel of the present invention desirably provides the capability of self-deflagration similar to a solid

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monopropellant. In addition, the high oxygen balance fuel of the present invention permits the use of much lower concentrations of oxidizer components and results in a much lower concentration of solid combustion products and greater gas output, which is particularly advantageous for volume limited systems. As a result, the high oxygen balance fuel of the present invention has applications in both of the systems set forth above and illustrated generally in Figures 1 and 2.

Although the yellow colored solid reaction product of aminoguanidine nitrate and nitric acid, as well as the yellow colored solid reaction product of nitric acid and other aminoguanidine salts, such as aminoguanidine bicarbonate and/or aminoguanidine sulfate, is assumed to be azodiformamide dinitrate (azobisformamide dinitrate), this invention is not limited only to this specific high oxygen balance fuel. The invention is also directed specifically to azodiformamide dinitrate (azobisformamide dinitrate). However, for simplicity, use of the term AZODN below refers both to the reaction product and azodiformamide dinitrate in anhydrous and hydrous versions, unless specifically indicated otherwise. Similar results would also be obtained by utilizing the azodiformamide dinitrate formed from the reaction of nitric acid and aminoguanidine bicarbonate and/or aminoguanidine sulfate.

A comparison of the high oxygen balance fuel of the present invention, namely, AZODN, with other high oxygen balance fuels (HOB and CAPS), shows that AZODN has a higher oxygen balance to carbon dioxide and water than other high oxygen balance fuels, as provided in Table 1.

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TABLE 1
Oxygen balance to CO₂ and H₂O for HOB Fuels

<u>Compound</u>	<u>Oxygen Balance to</u> <u>CO₂ and H₂O</u>
Azobisformamidine dinitrate (AZODN), C ₂ H ₈ N ₈ O ₆	-13.3%
Ethylenediamine dinitrate (EDDN), C ₂ H ₁₀ N ₄ O ₆	-25.8%
Guanidine nitrate (GN), CH ₆ N ₄ O ₃	-26.2%

The better oxygen balance of AZODN of the present invention over that of other high oxygen balance fuels, such as guanidine nitrate, permits the use of a lower concentration of oxidizer to maintain a desired .90/1 to 1.1/1 oxygen to fuel (O/F) balance in a resulting gas generant composition. However, if a gas generant is desired that is totally or essentially free of solid combustion product, an oxidizer, such as either phase stabilized or non-phase stabilized ammonium nitrate, can be utilized with the high oxygen balance fuel of the present invention. In such a case, the fuel of the present invention should be present as 40-60 wt% of the total gas generant composition. The use of AZODN of the present invention in either the form of the reaction product of aminoguanidine nitrate and nitric acid or, specifically, azobisformamidine dinitrate, produces higher gas outputs and less solid combustion products.

As provided in Table 2 below, the prior art fuels, such as 5-aminotetrazole (5ATZ)(discussed above in the Background of the Invention), guanidine nitrate (GN), and ethylenediaminedinitrate (EDDN), require a greater amount of strontium nitrate (SrN) in order to reach a .95/1 oxygen to fuel (O/F) balance. Moreover, gas generant compositions including these fuels produce less gas output and more solid combustion products than gas generant compositions including AZODN of the present invention.

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TABLE 2**Comparison of High Oxygen Balance (HOB) Fuels With SrN***

<u>Fuel</u>	<u>SrN/Fuel</u>	<u>Flame Temp. (K)</u>	<u>Gas Output</u>	<u>Solid Products</u>
AZODN	21.8/78.2	2734	32.4	12.5
EDDN	36.5/63.5	2546	32.4	17.9
GN	37.5/62.5	2236	30.6	21.6
5ATZ	37.9/62.1	2700	24.8	31.2

O/F=0.95/1

As demonstrated by the results set forth in Table 2, the compositions including EDDN, GN and 5ATZ required greater than 10% by weight more SrN than the composition including the high oxygen balance fuel (AZODN) of the present invention to provide the given 0.95/1 O/F ratio. Although 5ATZ exhibited a similar flame temperature as the present invention, the gas output was significantly lower and the content of solid combustion products was more than twice as high for the composition including 5ATZ as compared with the composition including AZODN.

If tailoring of the ballistics is anticipated, partial substitution of potassium perchlorate (KP) for strontium nitrate can be done. Under these conditions, the formation of solid combustion products decreases even further, as provided in Table 3.

TABLE 3**Partial substitution of KP for SrN with HOB Fuels**

<u>Fuel</u>	<u>SrN/KP/Fuel</u>	<u>Flame Temp. (K)</u>	<u>Gas Output</u>	<u>Solid Products</u>
AZODN	10.0/10.2/79.8	2792	32.9	11.2
EDDN	17.1/17.1/65.8	2615	32.6	17.6
GN	17.6/17.6/64.8	2304	32.7	18.1

Still, however, compositions including EDDN and GN as fuel, required significantly more potassium perchlorate and strontium nitrate than in the composition including AZODN. Although the gas output for all

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three of the above compositions were similar to one another, the solid combustion products production for the composition utilizing AZODN was much lower. Consequently, the gas generant of the present invention including AZODN is preferred for pyrotechnic gas generator systems as illustrated in Figures 1 and 2.

Compositions including the high oxygen balance fuel of the present invention (AZODN) and oxidizers are provided below in Tables 4-7 for accomplishing the desired O/F balance of 0.90/1 to 1.1/1. Specifically, compositions including AZODN and ammonium nitrate (AN) are provided in Table 4; AZODN, ammonium perchlorate (AP) and strontium nitrate (SrN) are provided in Table 5; AZODN, ammonium perchlorate (AP) and sodium nitrate (SN) are provided in Table 6; and AZODN, ammonium perchlorate (AP) and potassium nitrate (KN) are provided in Table 7. It should be noted that, although the compositions of Table 4 are hygroscopic, the production of solid combustion products is still very nil. In addition, the use of phase stabilized ammonium nitrate is preferred.

TABLE 4
AZODN and Ammonium Nitrate Compositions

<u>AZODN(wt%)</u>	<u>AN(wt%)</u>	<u>O/F Balance</u>
75	25	.9/1
67.35	32.65	.95/1
60	40	1.0/1
52.94	47.06	1.05/1
46.15	53.85	1.1/1

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TABLE 5
AZODN, Ammonium Perchlorate, and Strontium Nitrate
Compositions

	<u>AZODN(wt%)</u>	<u>AP(wt%)</u>	<u>SrN</u>	<u>O/F Balance</u>
5	82.3	9.3	8.4	.9/1
	77.4	11.9	10.7	.95/1
	72.9	14.3	12.8	1.0/1
	69.2	16.5	14.3	1.05/1
	64.8	18.5	16.7	1.1/1

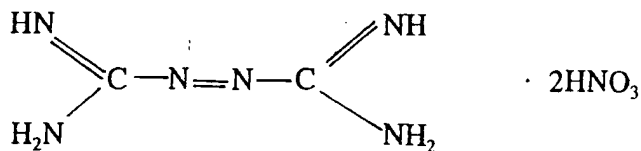
10 **TABLE 6**
AZODN, Ammonium Perchlorate, and Sodium Nitrate Compositions

	<u>AZODN(wt%)</u>	<u>AP(wt%)</u>	<u>SN</u>	<u>O/F Balance</u>
	83.7	9.5	6.8	.9/1
	79.1	12.1	8.8	.95/1
15	74.8	14.6	10.6	1.0/1
	70.8	16.9	12.3	1.05/1
	67.0	19.1	13.9	1.1/1

20 **TABLE 7**
AZODN, Ammonium Perchlorate, and Potassium Nitrate
Compositions

	<u>AZODN(wt%)</u>	<u>AP(wt%)</u>	<u>KN</u>	<u>O/F Balance</u>
	82.6	9.3	8.1	.9/1
	77.8	11.9	10.3	.95/1
	77.3	14.3	12.4	1.0/1
25	69.2	16.5	14.3	1.05/1
	65.3	18.6	16.1	1.1/1

In order to better understand the function of the high balance fuel of the present invention, examples of theoretical reactions of AZODN of the present invention are provided below wherein the structural formula for the AZODN is as follows:

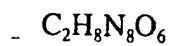


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and the molecular formula is:



(1) Neat AZODN as a monopropellant for use in hybrid or ignition systems:

5	$\text{C}_2\text{H}_8\text{N}_8\text{O}_6 \rightarrow$	$4\text{H}_2\text{O} +$	$2\text{CO} +$	4N_2
	240	72	56	112 = 240
	100.0%	30.0%	23.33%	46.67%
		1.667 M	0.833 M	1.667 M

Total Gas Output: 100.0 Wt. %

10 Total Gas Output (Moles): 4.167 Moles/100 Gms.

Total Solid Combustion Products: Zero Wt. %

(2) AZODN with ammonium nitrate (normal or phase stabilized):

	$2\text{C}_2\text{H}_8\text{N}_8\text{O}_6 + 3\text{NH}_4\text{NO}_3 \rightarrow$	$14\text{H}_2\text{O} +$	$3\text{CO}_2 +$	$\text{CO} +$	11N_2
	480	240	252	132	28 308 = 720
15	66.67%	33.33%	35.00%	18.33%	3.89% 42.78%
			1.944M	0.417M	0.139M 1.528M

Total Gas Output: 100.0 Wt. % (O/F=1.00) 100.0 Wt. %
(O/F=0.95)

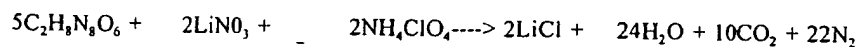
Total Gas Output (Moles): 4.04 Moles/100 Gms.

20 Total Solid Combustion Products: Zero Wt. %

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(3) AZODN with lithium nitrate and ammonium perchlorate:

1200	138	234	84	432	440	616	=1572
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76.33%	8.78%	14.89%	5.34%	27.48%	27.99%	39.19%	
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5

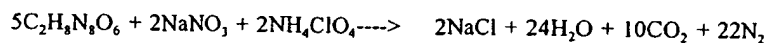
0.127M 1.53M 0.636M 1.400M

Total Gas Output: 94.7 Wt% (O/F=1.00) 95.6 Wt% (O/F=0.95)

Total Gas Output (Moles): 3.69 Moles/100 Gms.

Total Solid Combustion Products: 5.3 Wt.% (O/F=1.00) 4.4 Wt% (O/F=0.95)

10

(4) AZODN with sodium nitrate and ammonium perchlorate:

1200	170	234	116	432	440	616	=1604
------	-----	-----	-----	-----	-----	-----	-------

74.81%	10.60%	14.59%	7.23%	26.93%	27.43%	38.41%	
--------	--------	--------	-------	--------	--------	--------	--

0.125M 1.50M 0.623M 1.372M

15

Total Gas Output: 92.8 Wt% (O/F=1.00) 93.8 Wt% (O/F=0.95)

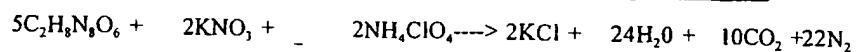
Total Gas Output (Moles): 3.50 Moles/100 Gms

Total Solid Combustion Products: 7.2 Wt% (O/F=1.00) 6.2 Wt% (O/F=0.95)

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(5) AZODN with potassium nitrate and ammonium perchlorate

1200	202	234	148	432	440	616 = 1636
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73.35%	12.35%	14.30%	9.05%	26.41%	26.89%
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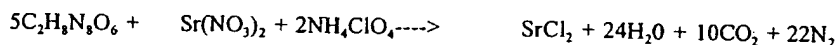
37.65%

0.122M 1.467M 0.611M 1.38M

Total Gas Output: 91.0 Wt% (O/F=1.00) 92.0 Wt% (O/F=0.95)

Total Gas Output (Moles): 3.42 Moles/100 Gms

Total Solid Combustion Products: 9.0Wt% (O/F=1.00) 8.0 Wt% (O/F=0.95)

(6) AZODN with strontium nitrate and ammonium perchlorate:

1200	212	234	157	432	440	616 = 1645
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72.90%	12.89%	14.21%	9.54%	26.26%	26.75%	37.45%
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0.061M 1.459M 0.608M 1.338M

Total Gas Output: 90.5 Wt% (O/F=1.00) 92.0 Wt% (O/F=0.95)

Total Gas Output (Moles): 3.405 Moles/100 Gms.

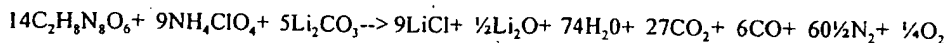
Total Solid Combustion Products: 9.5 Wt% (O/F=1.00) 8.0 Wt% (O/F=0.95)

(7) AZODN with lithium carbonate coolant and ammonium perchlorate:

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3360 1053 370 = 378 15 1332 1188 168 1694
8 =4783

70.25% 22.01% 7.74% 7.90% 0.31% 27.85% 24.84% 3.51% 35.42%
0.17%

.188M .010M 1.547M .565M .125M 1.265M

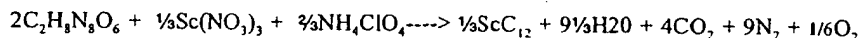
.005M.

Total Gas Output: 91.79 Wt% (O/F=1.00) 9 2 . 0 0 W t %
(O/F=0.95)

Total Gas Output (Moles): 3.51 Moles/100 Gms. 3 . 7 3
Moles/100 Gms

Total Solid Combustion Products: 8.20 Wt.% (O/F=1.00) 8.00 Wt.%
(O/F=0.95)

(8) AZODN with scandium nitrate and ammonium perchlorate:



480 77 78 38 167.4 176 251 2.6
=635

75.59% 12.13% 12.28% 5.98% 26.36% 27.72% 39.53%
0.41%

0.05M. 1.46M. 0.63M. 1.41M.

0.01M

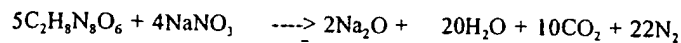
Total Gas Output: 94.0 Wt.% (O/F=1.00) 3.51 Moles/100 Gms
(O/F=1.00)

Total Solid Combustion Products: 6.0 Wt.% (O/F=1.00)

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(9) AZODN with sodium nitrate:

1200	340	124	360	440	616	= 1540
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77.92%	22.08%	8.05%	23.38%	28.57%	40.00%
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5

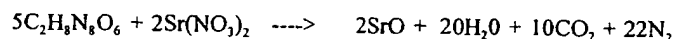
0.130M 1.299M 0.649M 1.429M

Total Gas Output: 92.0 Wt.% (O/F=1.00) 93.0 Wt.% (O/F=0.95)

Total Gas Output (Moles): 3.38 Moles/100 Gms.

Total Solid Combustion Products: 8.0 Wt.% (O/F=1.00) 7.00 Wt.% (O/F=0.95)

10

(10) AZODN with strontium nitrate:

1200	424	208	360	440	616	= 1624
------	-----	-----	-----	-----	-----	--------

73.89%	26.11%	12.81%	22.17%	27.09%	37.93%
--------	--------	--------	--------	--------	--------

0.123M 1.232M 0.616M 1.355M

15

Total Gas Output: 87.2 Wt.% (O/F=1.00) 89.3 Wt.% (O/F=0.95)

Total Gas Output (Moles): 3.20 Moles/100 Gms.

Total Solid Combustion Products: 12.8 Wt.% (O/F=1.00) 10.7 Wt.% (O/F=0.95)

20

(11) AZODN with potassium perchlorate:

480	138	74	144	176	224	= 618
-----	-----	----	-----	-----	-----	-------

77.67%	22.33%	11.97%	23.30%	28.48%	36.25%
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0.162M 1.294M

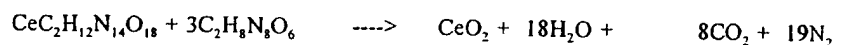
0.647M 1.295 M

Total Gas Output: 88.03 Wt.% (O/F=1.00) 89.90 Wt.%
(O/F=0.95)

Total Gas Output (Moles): 3.24 Moles/100 Gms. 3.56
Moles/100 Gms

Total Solid Combustion Products: 11.97 Wt.% (O/F=1.00) 10.10 Wt.%
(O/F=0.95)

(12) AZODN with aminoguanidine hexanitratocerate:



660 720 172 324 352 532 = 1380

47.82% 52.18% 12.46% 23.48% 25.51% 38.55%

= 100%

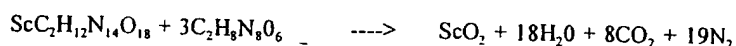
Total Gas Output: 87.54%

Total Solid Combustion Products: 12.46%

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(13) AZODN with aminoguanidine hexanitratoscandate:

565	720	77	324	352	532	= 1285
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43.97%	56.03%	5.99%	25.21%	27.39%	41.40%	= 100%
--------	--------	-------	--------	--------	--------	--------

5 Total Gas Output: 94.01%

Total Solid Combustion Products: 5.99%

As provided by the above theoretical reactions of AZODN, a substantial gas output is possible by utilizing the fuel of the present invention. In most cases, the gas output is over 90 wt%. Even at the greater level of solid combustion products formed, the gas generant of the present invention utilizing AZODN produces less solid combustion products than prior art gas generant compositions.

The specific process of obtaining the resulting reaction product of the present invention from the reaction of aminoguanidine nitrate and nitric acid is provided below. Further, use of this resulting reaction product with various additives are also provided to demonstrate the advantageous features thereof. Consequently, the term AZODN as used in Examples 1-12 provided below refers to the actual yellow precipitate of Example 1. As noted above, the reaction product of nitric acid and other aminoguanidine salts, such as aminoguanidine bicarbonate or aminoguanidine sulfate, would provide substantially the same results as the AZODN utilized in the following examples. This is substantiated by the additional tests conducted to demonstrate that the product resulting from the reaction of nitric acid and these additional salts has the same characteristics as the AZODN of Example 1.

Example 1

The high oxygen balance fuel of the present invention was prepared by the following method. First, 10 grams of aminoguanidine nitrate (AGN)

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was weighed into a 400 ml glass beaker. Then, water, preferably distilled, up to about 20-25 ml volume was added whereupon a slurry of AGN/water resulted. A dispersion was formed by slowly pouring 150 ml of reagent grade nitric acid (70%), while stirring, into the AGN/water slurry, which brought the total volume up to about 170-175 ml. A 10 degree temperature rise occurred as the acid was first added. As the acid was continually added, the temperature came back down. The dispersion was then heated to 55-65°C with moderate stirring on a hot plate. This caused any remaining AGN to go into solution.

Heating was continued at 55-65°C during which time the solution went through a color transition from a water-white color to a straw color to an intensely bright yellow color (resembling the color of a solution of potassium dichromate). [Use of a hood and a ready ice bath are strongly suggested.] Moreover, the reaction should be limited to a temperature ceiling of below 65°C. It should be noted that the solution will turn a deeper yellow color just before exotherming.

The beaker was then placed in an ice bath to cool down the contents and allow the effervescence to subside. A yellow precipitate appeared as the temperature dropped below 12°C after the reaction mixture was held in the ice bath at about 0-5°C. The yellow precipitate was vacuum filtered and washed with several rinses of distilled water. The precipitate was then washed several times with ethanol and then dried at 62°C.

Example 2

The infrared absorption spectra for the reaction product formed from the procedure set forth in Example 1 was determined and is provided in Figure 3. The absorption spectra was compared with the infrared absorption spectra of azodicarbamidine dinitrate found in the literature, *Anal. Chem.* 23, 1594 (1951). A comparison of Figure 3 with the reference spectra (Figure 11) showed that the synthesized azobisformamidine-type

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reaction product of the present invention is considered to be 1,1'-azodiformamidine dinitrate (azodicarbamidine dinitrate).

Example 3

Differential scanning calorimetry (DSC) was used to compare the thermal stability of the washed reaction product of Example 1 and a thermally aged reaction product (17 days at 107°C). The DSC plots for the washed reaction product and the thermally aged reaction product showed that aging only slightly changed the material's exotherm peak and the material's exotherm onset. Specifically, the exotherm onset changed from 160.82°C to 170.21°C and the exotherm peak changed from 183.32°C to 185.47°C. Consequently, the AZODN fuel of the present invention exhibits good aging characteristics.

Example 4

Neat AZODN powder, produced by the method of Example 1, containing no oxidizers or other additives, self-deflagrated very rapidly when ignited at ambient temperature and pressure. Specifically, a small quantity (1/2 gram) of the high oxygen balance fuel of Example 1 was placed in a heap in the center of a watch glass and the flame of a burning splint was impinged on the sample. The sample immediately ignited and combusted very rapidly and cleanly similar to smokeless rifle powder. Such rapid self-deflagration makes the AZODN fuel of the present invention very beneficial for use in heterogeneous and/or hybrid inflators or auto-ignition pills (AIP's) and all-pyro gas generating systems.

Example 5

A 0.269 gram quantity of AZODN of the present invention was placed in a pre-weighed aluminum pan and ignited with a burning splint. The pan was reweighed after igniting. Of the initial AZODN reaction product 0.005 grams of a tan residue remained, leaving a burn residual of 1.84% by weight.

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Additional tests were performed on small propellant batches containing the AZODN reaction product of the present invention for determining sensitivity, thermal aging, weight loss, and ballistics properties. The density of the product and propellants made from the product was determined from the weight and pellet dimension measurements to be 1.66 g/cc or greater.

Example 6

When 1/4 inch x 5/8 inch pressed pellets of neat AZODN of the present invention were burned in a strand bomb, without any oxidizer or other additives, they exhibited burning rates of 0.122, 0.342, and 0.428 inches per second (ips) at 100, 500, and 750 psi, respectively. These rates yielded a burning rate exponent of 0.63.

Example 7

A propellant (Batch #11899) containing 10.60% sodium nitrate (SN) as an oxidizer and scavenger, 14.59% ammonium perchlorate (AP), and 74.81% AZODN of the present invention was formulated at an O/F ratio of 1.0 to provide, when combusted, 7% solid combustion products and 3.7 moles of substantially non-toxic gas per 100 grams of composition product. This formulation gave burning rates of 0.32 and 0.46 ips, respectively, at 500 and 750 psi. These rates yielded a pressure exponent of 0.90.

Example 8

Another propellant (Batch #11900) containing 22.05% sodium nitrate (SN) oxidizer and 77.92% AZODN of the present invention was formulated to provide, when combusted, an 8% solid combustion products level and 3.4 moles of substantially non-toxic gas per 100 grams of composition. When 1/4 x 5/8 inch pellets were tested for ballistic properties, burning rates at 250, 500, 750, 1000 and 1250 psi were respectively 0.17, 0.32, 0.47, 0.59, and 0.73 ips. These values yielded a pressure exponent of 0.90.

Example 9

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Another propellant (Batch #11901) containing 7.74% lithium carbonate (LC) scavenger and coolant, 22.01% AP oxidizer, and 70.25% AZODN of the present invention provided a burning rate of 0.34 ips at 500 psi but suffered severe weight loss of 5.9% after 24 hours at 107°C. The DSC for this formulation provided an onset temperature of 146°C and an exotherm peak at 179°C.

Example 10

A propellant (Batch #11903) containing weight percents of 12.35% potassium nitrate (KN) acting as a scavenger/oxidizer, 14.3% ammonium perchlorate (AP), and 73.35% AZODN of the present invention was formulated at an O/F ratio of 1.0 to provide on combustion, a theoretical solid combustion products level of 9% and 3.6 moles of substantially non-toxic gas per 100 grams of composition. When pressed into 1/4 x 5/8 inch pellets and tested for ballistic properties, the formulation gave a burning rate of 0.40 and 0.52 ips at 500 and 750 psi, respectively, with a pressure exponent of 0.56.

Example 11

Another propellant (Batch #11905) containing 12.89% strontium nitrate (SrN), 14.21% AP, and 72.90% AZODN of the present invention was formulated (with SrN acting as a clinker/scavenger/oxidizing agent) at an O/F ratio of 1.0 to provide, when combusted, a solid decomposition product level of 9.5% resulting in 3.5 moles of substantially non-toxic gas per 100 grams of composition. This mixture gave a burning rate of 0.34 and 0.61 ips at 500 and 1000 psi with a pressure exponent of 0.85.

Onset temperatures and exotherm peaks for the various propellant mixtures provided above are given in Table 8. These temperatures were obtained from DSC plots conducted for each of the above-noted batches.

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TABLE 8**Exotherm Peak and Exotherm Onset Temperatures Observed via DSC**

	<u>Batch</u> <u>(°C)</u>	<u>Component</u>	<u>Composition(wt%)</u>	<u>Onset (°C)</u>	<u>Peak</u>
5	Neat	AZODN	100	161	183
	B11899	AZODN	74.8	158	182
		SN	10.6		
		AP	14.6		
10	B11900	AZODN	77.9	158	181
		SN	22.1		
	B11901	AZODN	70.3	146	179
		LC	7.7		
		AP	22.0		
15	B11903	AZODN	73.35	157	183
		KN	12.35		
		AP	14.3		
	<u>Batch</u> <u>(°C)</u>	<u>Component</u>	<u>Composition(wt%)</u>	<u>Onset (°C)</u>	<u>Peak</u>
20	B11905	AZODN	72.9	160	184.5
		SrN	12.9		
		AP	14.2		

The pressurized burn rates for the above Examples of AZODN propellants are provided below in Table 9.

TABLE 9**Pressurized Burn Rates for AZODN Propellants**

		Burning Rate						
		Pressure	Inches per second at Pressure (Psia)					
<u>Batch</u>	<u>Exponent</u>		<u>100</u>	<u>250</u>	<u>500</u>	<u>750</u>	<u>1000</u>	<u>1250</u>
30	Neat AZODN	0.63	0.12	----	0.34	0.43	----	----
	B11899	0.90	----	----	0.32	0.46	----	----

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B11900	0.90	----	0.17	0.32	0.47	0.59	0.73
B11903	0.56	----	----	0.40	0.52	----	----
B11905	0.85	----	----	0.34	----	0.61	----

Weight loss during aging is presented in Table 10 for the various
AZODN formulations provided above.

TABLE 10

Pellet Weight Loss
Vs. Days at Temperature

	<u>Batch</u>	<u>Days at Temperature</u>	Cumulative Weight Loss at Temperature	
			90°C (%)	107°C (%)
10	Neat AZODN	1	0.16	0.60
		3	0.41	1.09
		7	0.58	1.48
		13	0.64	1.65
		25	0.87	1.79
15	B11899	1	0.27	0.54
		2	0.57	0.83
		3	0.62	0.98
		7	0.88	1.30
		16	1.08	1.66
20	B11903	1	0.27	0.44
		2	0.39	0.62
		3	0.44	0.66
		7	0.61	0.96
		16	0.74	1.16
25	B11905	1	0.23	0.43
		2	0.36	0.61
		3	0.42	0.78
		7	0.60	1.11
		16	0.78	1.43
30		1		
		2		
		3		
		7		
		16		

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Each of the above examples used filtered, washed and dried but unrecrystallized AZODN. Table 10 shows that very little weight is lost during accelerated aging at 107 and 90°C. The pellets (½ inch in diameter x ½ inch in height) were dried at 62°C (without a vacuum) prior to placing in either aging oven. Some weight loss occurs during the first day (24 hours) and is likely due to aqueous or non-aqueous volatile content.

Example 12

Reformulation of the above propellant batches at an O/F ratio of 0.90 and 0.95 resulted in solid combustion products levels in the range of 6 to 7½%. Substitution of SN for a KN scavenger and oxidizer in AP/AZODN systems (where the scavenger inhibits and/or eliminates formation of hydrogen chloride) resulted in solid combustion products levels of 6 and 4½% at O/F ratios of 0.95 and 0.90, respectively.

All of the propellant batches utilizing the high oxygen balance fuel of the present invention, as well as neat AZODN, when tested, responded with acceptable hazards properties with respect to impact, friction, and electrostatic sensitivity performed on powders. All initial propellant impact tests showed 10 negatives at 2.0 kg at 50 cm (100 kg-cm). Later tests with drier ingredients indicated acceptable hazards properties. However, the impact test values from these later tests indicated somewhat greater sensitivity, e.g. 50 kg-cm. All electrostatic discharge tests showed 10 negatives at six joules and 5kV. All friction tests (type ABL) showed 10 negatives at 300 psi-90° with LC, SN and KN propellants (see examples below) showing 10 negatives at 1800 psi-90°.

Thermal stability studies, which included differential scanning calorimetry (DSC) and accelerated aging at elevated temperatures, were conducted on several batches containing the high oxygen balance product believed to be AZODN prepared according to Example 1. A DSC plot of a propellant respectively containing 12.9, 14.2, and 72.9 weight percentages of strontium nitrate (SrN), ammonium perchlorate (AP), and

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unrecrystallized AZODN showed an exothermic onset occurring at 161°C with major decomposition at 184.5°C.

Differential scanning calorimetry (DSC) indicated the onset of exothermic decomposition to be about 160°C for all of the above propellants. This suggests that an auto-ignition pill (AIP) may not be necessary with propellants containing the high oxygen balance fuel of the present invention or AZODN. Because neat AZODN and propellants containing AZODN possess low, but acceptable auto-ignition temperatures and acceptable pressure exponents combined with high burning rates at low operating pressures, this invention will be very effective for use volume limited, reduced weight inflator hardware. In addition, if manufactured from aluminum, high performance plastics, or lower gauge steel components, operation of an inflator using the propellants of the present invention will more likely pass bonfire tests that require an inflator to burst without fragmenting.

Example 13

The high oxygen balance fuel of the present invention was prepared by the method of Example 1, but instead of aminoguanidine nitrate, aminoguanidine bicarbonate was combined with nitric acid to provide an embodiment 2 of the high oxygen balance fuel of the present invention.

Example 14

The high oxygen balance fuel of the present invention was prepared by the method of Example 1, but instead of aminoguanidine nitrate, aminoguanidine sulfate was combined with nitric acid to provide an embodiment 3 of the high oxygen balance fuel of the present invention.

Example 15

The high oxygen balance fuel of the present invention was prepared by the method of Example 1, but instead of aminoguanidine nitrate, aminoguanidine sulfate was combined with nitric acid. Further, the acid utilized in the method of Example 1 was used as the nitric acid component

to provide an embodiment 4 of the present invention. Consequently, the nitric acid can be recycled after the fuel of the present invention is recovered to improve the yield of the final product. The nitric acid used in one reaction can be used in a subsequent reaction no matter which aminoguanidine salt is used in the initial reaction or the subsequent reaction.

Figure 4 provides an additional DSC plot of the AZODN of Example 1. As can be seen from this Figure, the exothermic onset occurred at approximately 160°C with major decomposition at 185.1°C. Figure 5 shows a DSC plot of the fuel produced by Example 13 (Embodiment 2) with an exothermic onset occurring at 157.69°C and major decomposition at 184.98°C. Consequently, the fuel of Example 13 utilizing aminoguanidine bicarbonate is the substantially the same as the fuel of Example 1 and, thus, is azodiformamidine dinitrate. Use of aminoguanidine bicarbonate at the aminoguanidine salt is preferred in the present invention.

Figure 6 shows a DSC plot of the fuel produced by Example 14 (Embodiment 3) with an exothermic onset occurring at 150.39°C and major decomposition at 182.44°C. Consequently, the fuel of Example 14 utilizing aminoguanidine sulfate is also the substantially the same as the fuel of Example 1 and, thus, is azodiformamidine dinitrate.

Figures 7, 8 and 9 are IR spectras of the fuel of Examples 1, 13 and 14, respectively. Figures 10(a)-(d) are also IR spectra of the fuel of Examples 15, 1, 13 and 14, respectively. By comparing these spectras with the IR spectra of Figure 11 taken from Analytical Chemistry, Vol. 23, p. 1594 (1951), it can be seen that the high oxygen balance fuel of the present invention utilizing aminoguanidine salt, including aminoguanidine nitrate, aminoguanidine bicarbonate, and aminoguanidine sulfate, produces azodiformamidine dinitrate. The same is true with respect to the recycled acid of Example 15.

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Tables 11-14 are provided to show the use of representative AZODN made from aminoguanidine nitrate, aminoguanidine bicarbonate, or aminoguanidine sulfate, or combinations thereof. As can be seen from the results of Table 11, the total ash is production is low, flame temperatures are acceptable and the hazard tests are designated as "green" meaning acceptable. Specifically, Table 11 shows the AZODN propellant properties exhibited by five (5) different formulations without the use of a binder

Table 12 is an evaluation of the use of binders in AZODN propellant compositions and particularly comparing the use of QPAC-40 binder (polycarbonate) made by PAC Polymers, Inc. and CAB (cellulose-acetate butyrate) made by Eastman Chemical, Inc. This table generally shows that an increase in binder content increases the initial crush strength of the AZODN propellant composition.

Tables 13 and 14 demonstrate the effect of annealing time and fine particle size on the crush strength and burning rate of various AZODN propellant compositions with and without a QPAC-40 binder.

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TABLE II
AZODN PROPELLANTS W/O BINDERS

Formulation No: AZODN	AA-106 A	HIGH Rb COMPOSITIONS			VERY HIGH Rb NL-021698-1
		AA-106 B	B12020	12020/12019	
GN	78.0	79.10	39.00	37.15	81.25
AP	---	---	31.00	33.15	---
KP	11.70	12.01	15.85	16.42	---
KN	---	---	---	---	18.75
SN	10.30	---	14.15	7.08	---
	---	8.80	---	6.20	---
Total Ash %	7.5	6.0	10.0	9.0	10.1
Flame Temp., K	2777	2779	2563	2563	2809
Moles/Gas/100gms	3.7	3.7	3.7	3.8	3.5
<u>Ballistics</u>					
R _b @ 500 psi, ips	.35	.37	.31	---	.58
R _b @ 1000 psi, ips	.57	.67	.46	.43	1.02
Exponent, n	.70	.82	.62	---	.67
<u>400 hrs Aging @ 107°C</u>					
Crush Strength (Aged @ 107°C)	2038	3211	4114	2534	3351
Hazard Tests	Green	Green	Green	Green	Green

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TABLE 12

EVALUATION OF BINDERS IN ARCAIR-106 A AZODN PROPELLANT
COMPARISON OF QPAC-40 AND CAB

<u>Formulation No.</u>	<u>AA-106AQ1</u>	<u>AA-106AQ2</u>	<u>AA-106AQ3</u>	<u>AA-106AQ5</u>	<u>AA-106AC1</u>	<u>AA2-106AC3</u>	<u>AA-106 A</u>
AZODN	74.58	71.36	68.15	61.73	74.05	66.57	59.10
AP, 3μ	12.94	14.12	15.29	17.63	13.22	16.13	19.03
KN,-40mesh	11.48	12.52	13.56	15.64	11.73	14.30	16.87
QPAC40	1.00	2.00	3.00	5.00	---	---	---
CAB	---	---	---	---	1.00	3.00	5.00
							-39-
<u>Total Ash %</u>	8.5	9.2	10.0	11.5	8.6	10.5	12.6
<u>Flame Temp. °K</u>	2794	2785	2777	2759	2796	2783	2771
<u>Moles Gas/100gms</u>	3.6	3.6	3.6	3.5	3.6	3.6	3.5
<u>Crush Strength (initial)</u>	2732	3589	4872	6447	2728	3963	5354

TABLE 13

EFFECT OF ANNEALING TIME AND FINE PARTICLE SIZE ON CRUSH STRENGTH AND BURNING RATE OF ARCAIR-106 AZODN PROPELLANTS W & W/O QPAC-40 BINDER

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Formulation	AA106AWOB		AA106BWOB		AA106AQ1F		AA106BQ1F		AA106AQ2F		AA106BQ2F		AA106AQ3F		AA106BQ3F		AA106N		AA106NQ1		AA106CWOB		
AZODN	78.00	79.10	74.58	76.02	71.36	72.93	68.15	69.85	100.00	97.00	81.25												
GN	---	---	---	---	---	---	---	---	---	---	---												
AP,3μ	11.70	12.01	12.94	13.33	14.12	14.54	15.29	15.75	---	---	---												
KN,20μ	10.30	---	11.48	---	12.52	---	13.56	---	---	---	---												
SN 20μ	---	8.80	---	9.65	---	10.53	---	11.40	---	---	---												
QPAC-40	---	---	1.00	1.00	2.00	2.00	3.00	3.00	---	3.00	---												
KP	---	---	---	---	---	---	---	---	---	---	---												
SrN	---	---	---	---	---	---	---	---	---	---	18.75												
Total Ash %	7.5	6.0	8.5	6.7	9.2	7.2	10.0	7.8	Negligible	Negligible	10.1												
Flame Temp. °K	2777	2779	2794	2803	2785	2796	2777	2796	2480	2343	2809												
Moles Gas/100 gms	3.7	3.7	3.6	3.7	3.6	3.7	3.6	3.7	4.2	4.2	3.5												
Aging Cycling																							
Crush Strength(psi) (initial)	1999	1940	2388	3643	3769	3393	3963 ¹ , 8694 ²	4918, 7759 ²	2279	---	2003												
Crush Strength (Aged 400 hrs.@107°C)	---	---	---	---	---	---	3461	6166 ² , 6616 ³	2267	---	3351												
-40 to +107C Cycling (100 cycles)	---	1832	2388	3342	4708	4214	2929	5294	---	---	---												
-40 to +107C Cycling (200 cycles)	---	935	---	3294	---	4004	3345	4457	---	---	---												
Ballistics																							
Rb @ 500psi	.350	.355	---	.287	---	.295	---	.269	.34	.33	.58												
Rb @ 1000psi	.570	.633	---	.461	---	.509	.542	.491	.56	.55	1.02												
Rb @ 2000psi	---	---	---	---	---	.897	1.07	.897	---	.86	---												
Rb @ 4000 psi	---	---	---	---	---	---	1.72	---	---	---	---												
Exponent, n	.70	.83	---	.68	---	.82	.68 ³	.86	.63	.68	.67												
used -40 mesh KN																							
Annealed for 3 days @ 135°F instead of overnight																							
n = .68 @ 2000-4000 psi; n = 1.0 @ 1000-2000 psi																							

¹ used -40 mesh KN

² Annealed for 3 days @ 135°F instead of overnight

³ n = .68 @ 2000-4000 psi; n = 1.0 @ 1000-2000 psi

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TABLE 14

COMPARISON OF ARCAIR-106 B AZODN PROPELLANTS WITH AND W/O QPAC-40

<u>Formulation No:</u>	<u>AA-106B W/O Binder</u>	<u>AA-106BO1</u>	<u>AA-106BO2</u>	<u>AA-106BO3</u>
AZODN	79.10	76.02	72.93	69.85
AP, 3 μ	12.10	13.33	14.54	15.75
SN, Ground	8.80	9.65	10.53	11.40
QPAC 40	---	1.00	2.00	3.00
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<u>Total Ash %</u>	6.05	6.74	7.24	7.84
<u>Flame Temp., °K</u>	2826	2803	2796	2796
<u>Moles Gas/100g</u>	3.7	3.7	3.7	3.7
<u>Crush Strength (initial)</u>	2076	3643	3393	4918
<u>Burning Rate (ips @ 1000 psi)</u>	.67	.46	.51	.49

TABLE 15

SAMPLE ID	FIRE TEMP °F	INSOLUBLE WT.	SOLUBLE WT.	pH
B12020	70	0.83593g	3.4670g/-131mg	7.0
AA-106 A	70	1.23137g	1.5675g/+9mg	7.5
AA-106 A	70	1.30119g	1.5931g/-55mg	6.0
AA-106 A	70	0.61248g	0.7523g/-27mg	5.5
12020/12019	70	0.56786g	2.7353g/-65mg	6.1
AA-106 A	-40	0.49002g	1.5558g/-33mg	6.0
AA-106 A (inside)	-40	0.49058g		9.0
AA-106 A	-40	0.44710g	0.9576g	6.0
AA-106 B	-40	0.54327g	1.3217g	5.5

Table 15 shows the amount of insoluble and soluble decomposition product produced during an unfiltered inflator test of the gas generator propellant composition of the present invention made from the reaction of nitric acid and aminoguanidine salt, such as aminoguanidine nitrate, aminoguanidine sulfate, or the preferred salt, aminoguanidine bicarbonate. Specifically, the test involved a PD-67 full size heavy weight test hardware inflator firing unit without any filter collection system. The sample propellant was fired in a 60 liter tank and then rinsed to measure the amount of solid decomposition product in the tank. The pH of the resulting solid decomposition product was also obtained. As can be seen from the results set forth above in Table 15, the pH of the decomposition product is relatively neutral which is important to prevent harm to passengers of an automobile in which the propellant of the present invention is utilized during a collision in an air bag unit. Further, the amount of unfiltered insoluble and soluble decomposition product is relatively low.

As can be seen from the above Examples and corresponding testing, the high oxygen balance fuel of the present invention, preferably, azodiformamidine dinitrate, exhibits attractive propellant attributes and should be useful in a large number of pyrotechnic gas generant environments.

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What is claimed is:

1. A pyrotechnic gas generant composition comprising:

a high oxygen balance fuel, wherein said high oxygen balance fuel is a resulting solid yellow reaction product of nitric acid and an aminoguanidine salt.

2. A pyrotechnic gas generant composition of claim 1, wherein said aminoguanidine salt is selected from the group consisting of aminoguanidine bicarbonate, aminoguanidine sulfate and mixtures thereof.

3. A pyrotechnic gas generant composition of claim 2, said high oxygen balance fuel comprising 2-100% by weight of said pyrotechnic gas generant composition.

4. A pyrotechnic gas generant composition of claim 3, said high oxygen balance fuel comprising 40-100% by weight of said pyrotechnic gas generant composition.

5. A pyrotechnic gas generant composition of claim 2, wherein said resulting yellow reaction product of said aminoguanidine salt and nitric acid is prepared by a process comprising:

(a) providing said aminoguanidine salt;

(b) combining said aminoguanidine salt with nitric acid to form a dispersion, wherein said dispersion proceeds through a color transition from water white to straw to bright yellow color, said color being comparable to a potassium dichromate solution.

6. A pyrotechnic gas generant composition of claim 5, wherein 70% reagent grade nitric acid is combined with said aminoguanidine salt.

7. A pyrotechnic gas generant composition of claim 2, wherein said resulting yellow reaction product of said aminoguanidine salt and nitric acid is prepared by a process comprising:

(a) combining said aminoguanidine salt and water to form a slurry;

(b) stirring 70% nitric acid into said slurry to form a dispersion;

(c) heating said dispersion during which time said dispersion dissolves and proceeds with effervescence through a color transition from water white to straw to a bright yellow color to form a solution, said bright yellow color being comparable to a potassium dichromate solution;

5 (d) cooling said solution to precipitate said solid yellow reaction product.

8. A pyrotechnic gas generant composition of claim 7, wherein said dispersion is heated to 55-65°C and said solution is cooled to below 12°C.

10 9. A pyrotechnic gas generant composition of claim 2, further comprising at least one oxidizer, said oxidizer comprising from 0-98% by weight of said pyrotechnic gas generant composition.

10. A pyrotechnic gas generant composition of claim 9, wherein said at least one oxidizer comprises from 0-60% by weight of said pyrotechnic gas generant composition.

15 11. A pyrotechnic gas generant composition of claim 9, wherein said at least one oxidizer is substantially non-hygroscopic.

12. A pyrotechnic gas generant composition of claim 9, further including at least one additive selected from the group consisting of a scavenger, ignition aid, ignition initiator, gas conversion catalyst, ballistic modifier, slag formers, binders, energetic binders, plasticizers, energetic plasticizers, fuels, stabilizers, curing agents, cure catalysts, cross linkers, inorganic coolants, organic coolants and compounding aids and mixtures thereof.

25 13. A pyrotechnic gas generant composition of claim 9, wherein said at least one oxidizer is selected from the group consisting of non-metallic, alkali metal, alkaline earth metal, transition metal and transition metal complex nitrates, nitrites, chlorates, chlorites, perchlorates, chromates, or mixtures thereof.

30 14. A pyrotechnic gas generant composition of claim 13, wherein said oxidizer comprises sodium nitrate.

15. A pyrotechnic gas generant composition of claim 14, wherein said oxidizer further comprises ammonium perchlorate.

16. A pyrotechnic gas generant composition of claim 9, wherein said oxidizer comprises phase stabilized ammonium nitrate.

5 17. A pyrotechnic gas generant composition of claim 9, wherein said oxidizer comprises ammonium perchlorate, said composition further comprising an additive selected from at least one of the group consisting of ammonium perchlorate, ammonium nitrate, potassium perchlorate, strontium nitrate, potassium nitrate, lithium nitrate, lithium carbonate and mixtures thereof.

10 18. A pyrotechnic gas generant composition of claim 2, wherein said reaction product is crystallized or recrystallized.

19. A pyrotechnic gas generant composition of claim 1, further comprising at least one other high oxygen balance fuel.

15 20. A pyrotechnic gas generant composition of claim 19, wherein said other high oxygen balance fuel is selected from the group consisting of hydrazodicarbonamidine, diazoguanidine, formamidine, bisformamidine, azobisformamidine derivative fuels and mixtures thereof.

20 21. A pyrotechnic gas generant composition of claim 20, wherein said azobisformamidine derivative is selected from the group consisting of guanyl azide nitrate, diazoguanidine nitrate, azobisnitroformamidine, 1,1'-azodiformamidine dipicrate, and mixtures thereof.

22. A chemical delivery system for fire suppression comprising a vessel including:

25 a high oxygen balance fuel, wherein said high oxygen balance fuel is a resulting reaction product of an aminoguanidine salt and nitric acid; and a fire suppression chemical.

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23. A chemical delivery system for fire suppression of claim 22, wherein said aminoguanidine salt is selected from the group consisting of aminoguanidine bicarbonate, aminoguanidine sulfate, and mixtures thereof.

24. A method for inflating an article capable of retaining gas, comprising the steps of:

igniting a gas generant composition comprising a high oxygen balance fuel, wherein said high oxygen balance fuel is a yellow reaction product of an aminoguanidine salt and nitric acid;

generating gas and solid material as reaction products of said reaction of said high oxygen balance fuel;

passing said gas and solid material into a filter, retaining at least a portion of solid material on the filter, and allowing the gas to exit;

passing the filtered gas into an article, thereby filling or inflating the article.

25. A method of claim 24, wherein said aminoguanidine salt is selected from the group consisting of aminoguanidine bicarbonate, aminoguanidine sulfate and mixtures thereof.

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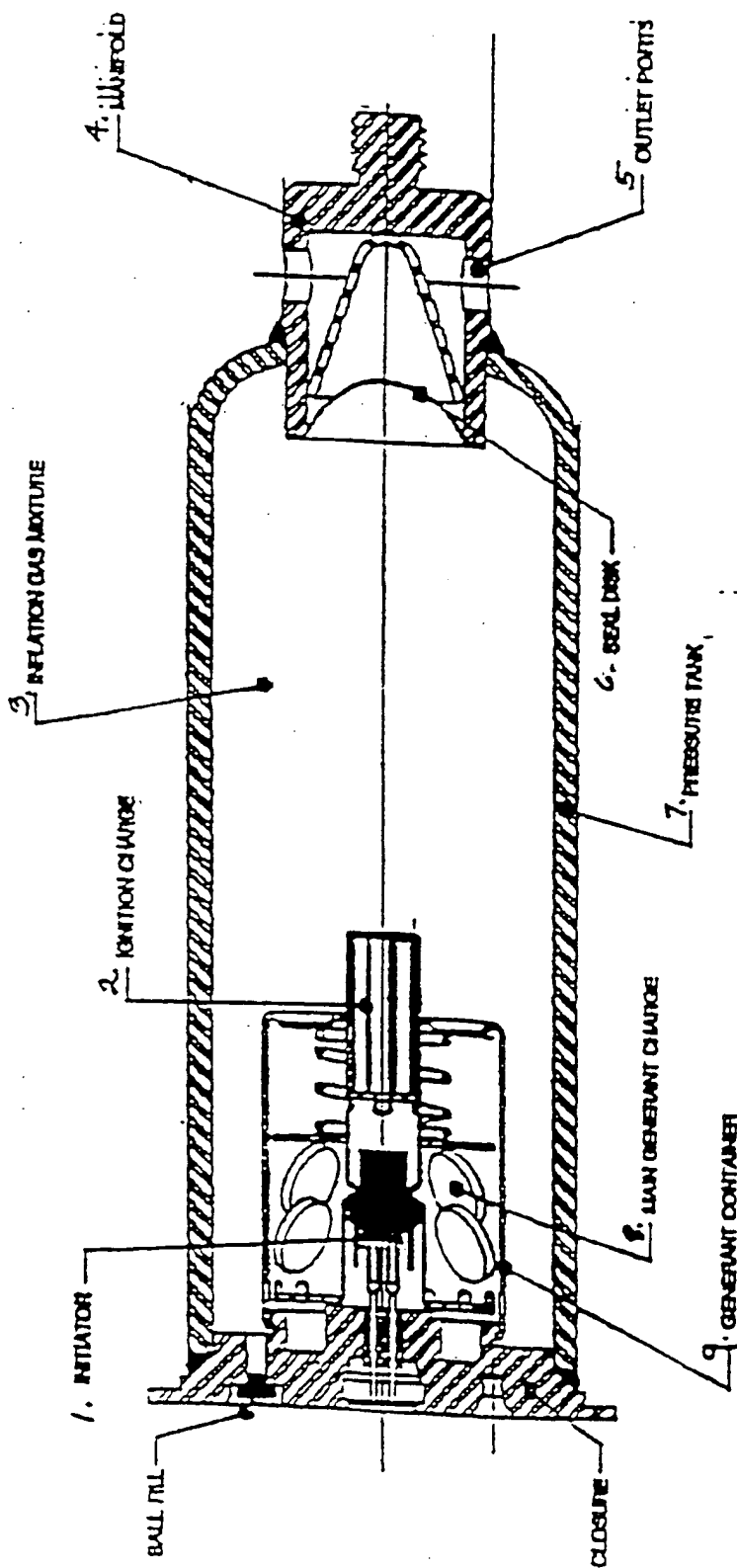


FIG. 1

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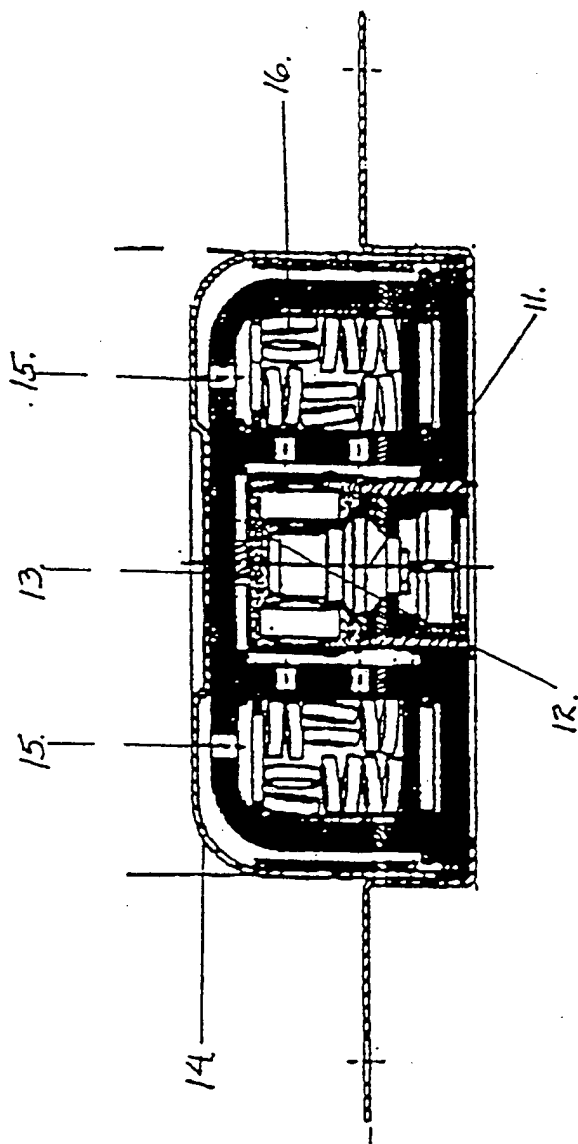


FIG. 2

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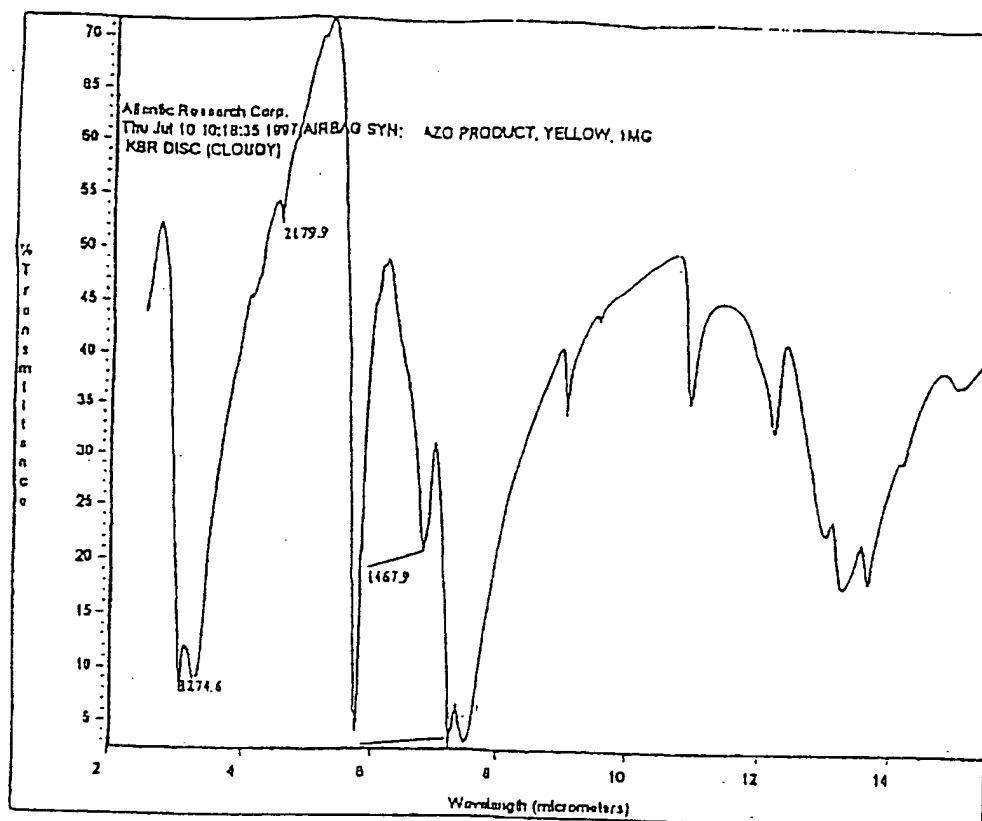


FIG. 3

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DSC

Sample: AIRBAG: A2 0291-31B-6
Size: 1.2400 g
Method: DSC 10 C/MIN
Comment: 10°C/MIN. 50ML/MIN N2 AL HER NOPH

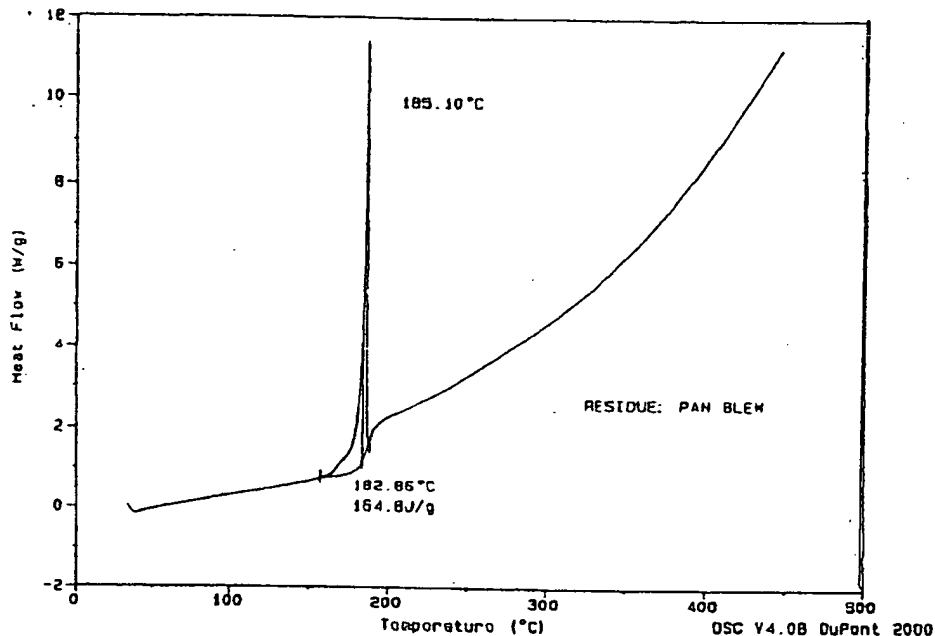


FIG. 4

Sample: AIRBAG: AZODIFORMAMIDINEINITRATE
Size: 1.1500 g
Method: STANDARD DSC 10C/MIN.
Comment: 10C/MIN, N2 50ML/MIN N2 AL HER NOPH. 0391-46A-1

DSC

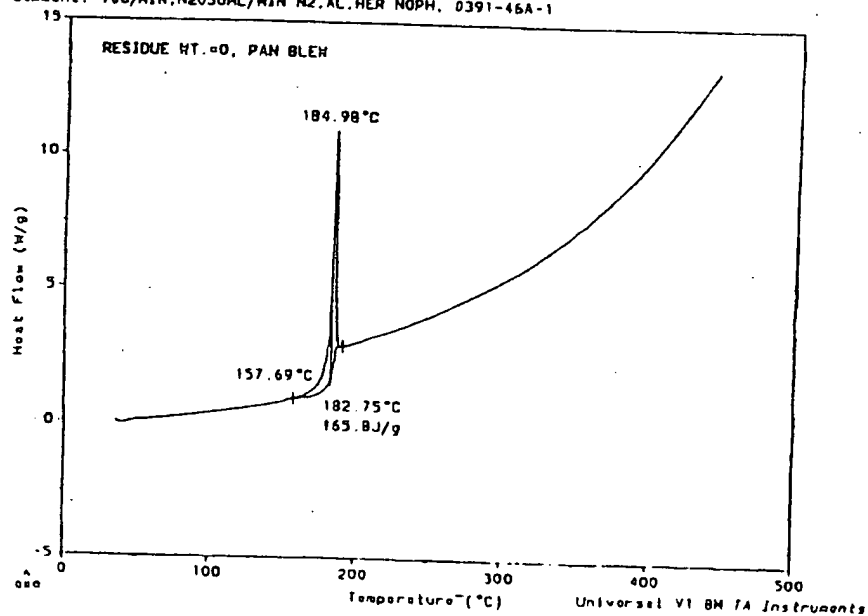


FIG. 5

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Sample: AIRBAG INQ; ACS, 391-608-1
Size: 1.6400 mg
Method: STANDARD DSC 10C/MIN.
Comment: 10C/MIN, N2850ML/MIN N2, AL, HER NOPH

DSC

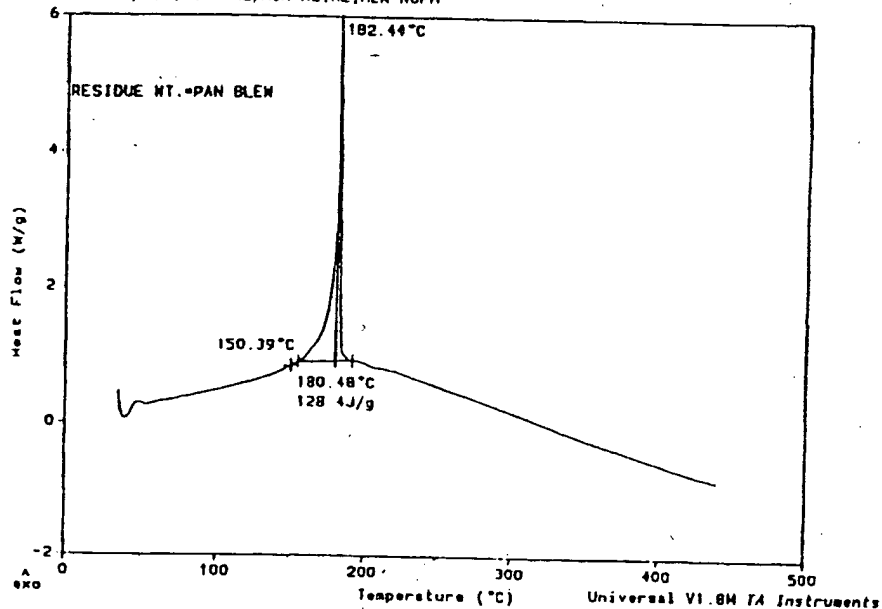


FIG. 6

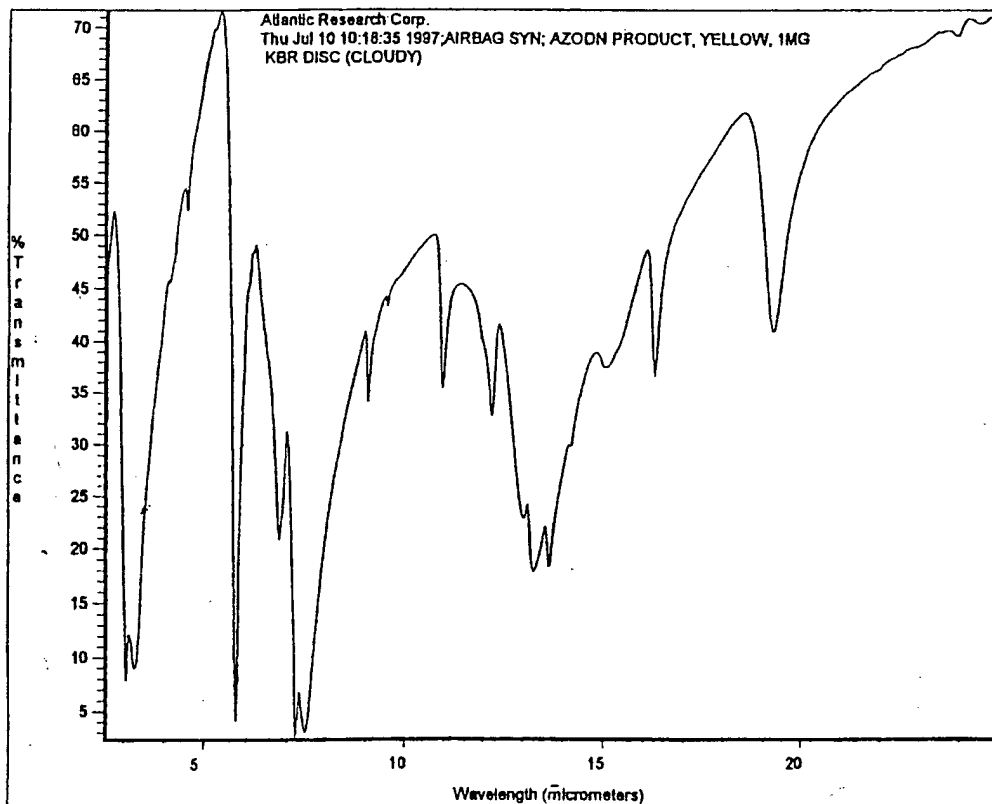


FIG. 7

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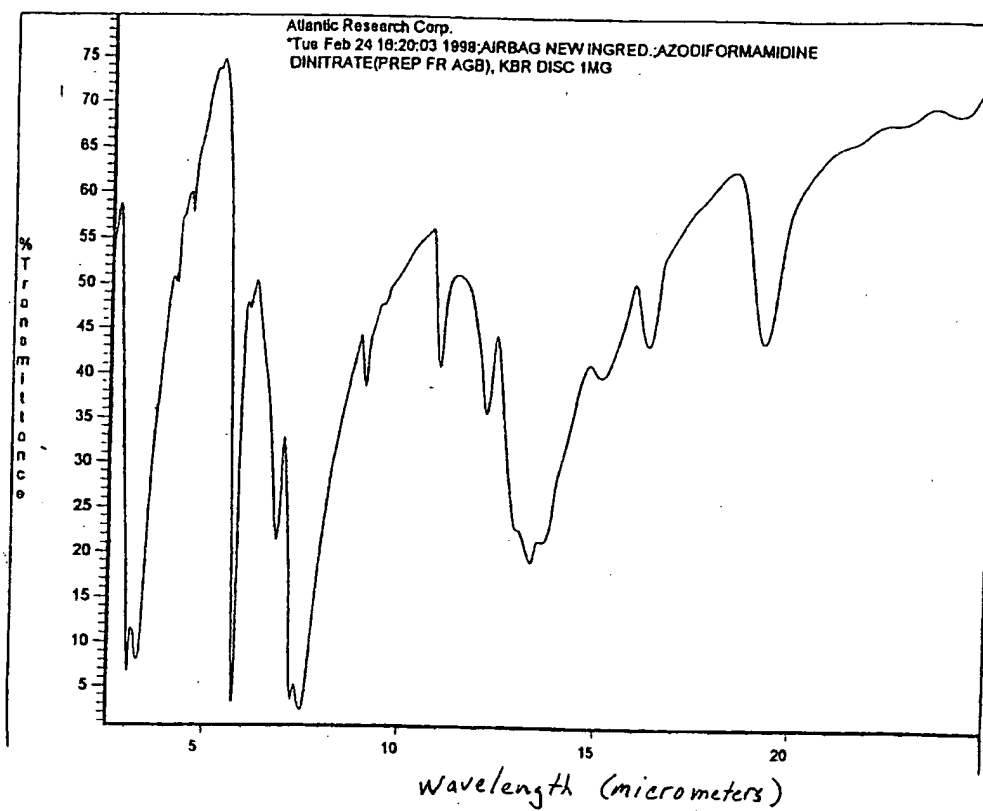


FIG. 8

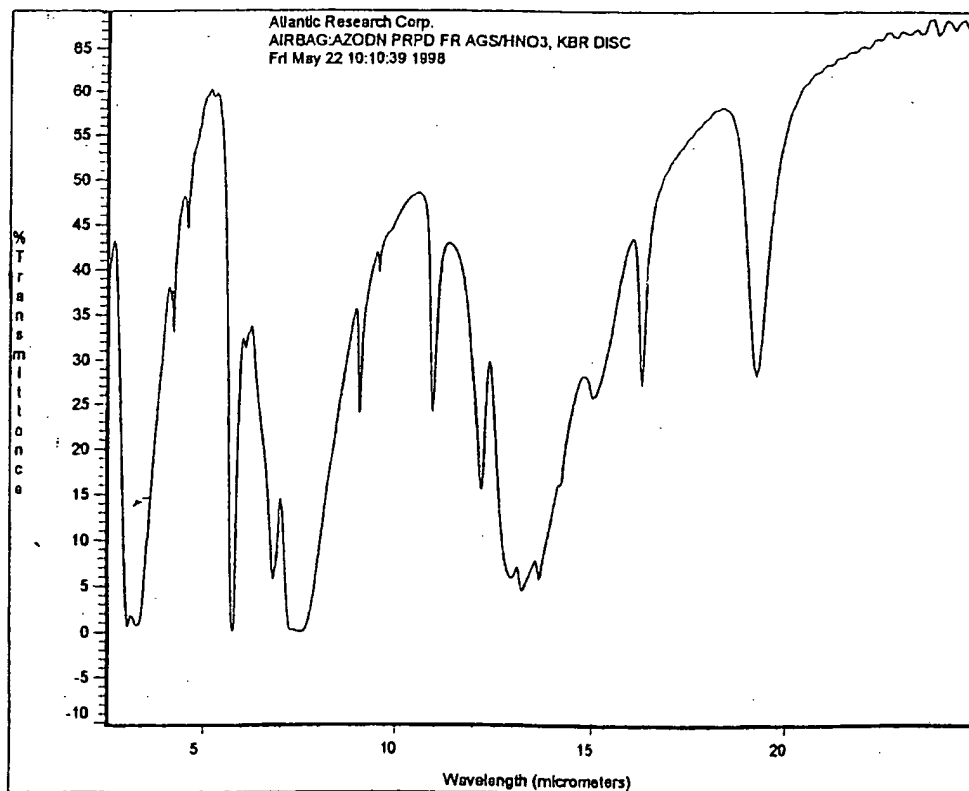


FIG. 9

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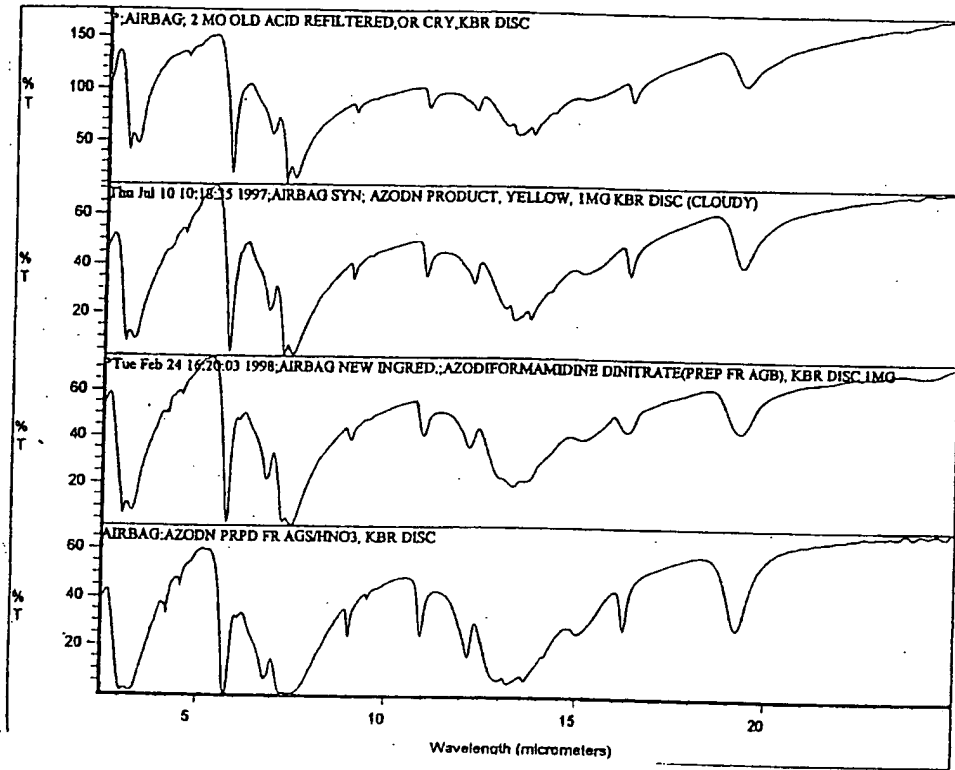


Fig. 10(a)

Fig. 10(b)

Fig. 10(c)

Fig. 10(d)

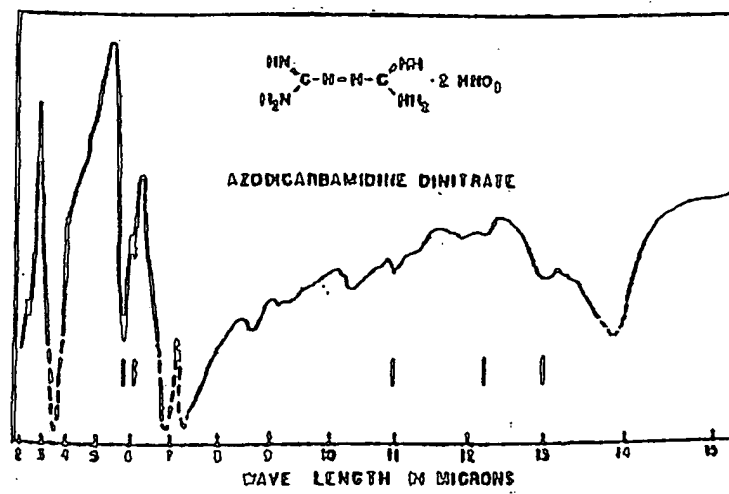


Fig. 11

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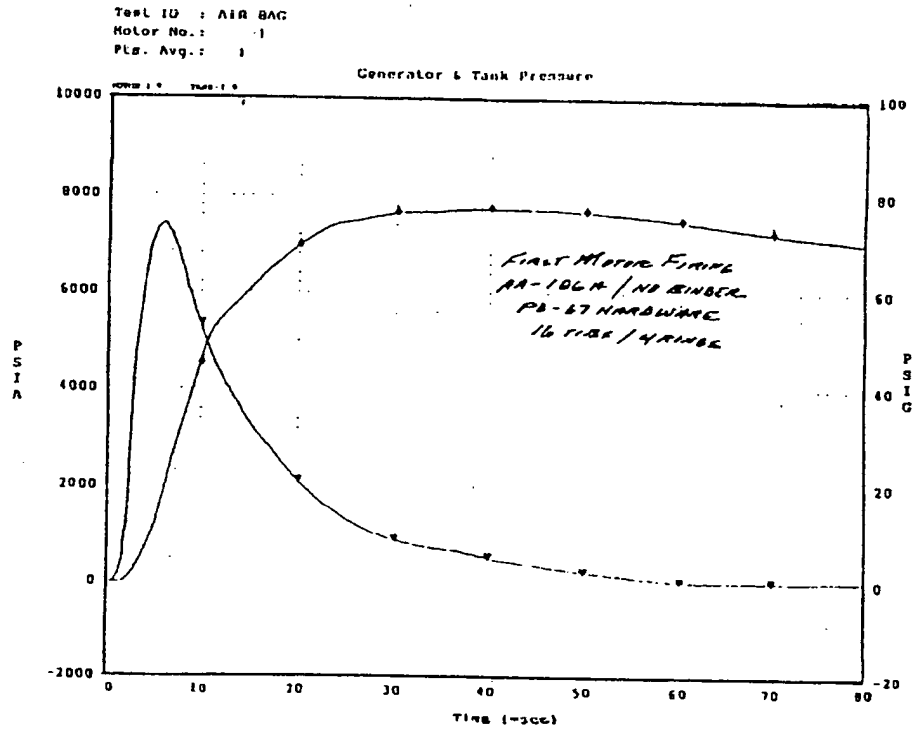


FIG. 12